Majtyka, Anna; Nowak, Anna; Marchand, Benoît; Chrobak, Dariusz; Ritala, Mikko; Räisänen, Jyrki; Nowak, Roman

Structure-Dependent Mechanical Properties of ALD-Grown Nanocrystalline BiFeO3 Multiferroics

Published in:
Journal of Nanomaterials

DOI:
10.1155/2016/5348471

Published: 01/01/2016

Please cite the original version:
Research Article

Structure-Dependent Mechanical Properties of ALD-Grown Nanocrystalline BiFeO₃ Multiferroics

Anna Majtyka, Anna Nowak, Benoît Marchand, Dariusz Chrobak, Mikko Ritala, Jyrki Räsänen, and Roman Nowak

1Nordic Hysitron Laboratory, Department of Materials Science and Engineering, Aalto University, 00076 Espoo, Finland
2A. Chelkowski Institute of Physics, University of Silesia, Uniwersytecka 4, 40-007 Katowice, Poland
3Department of Physics, University of Helsinki, P.O. Box 43, 00014 Helsinki, Finland
4Institute of Material Sciences, University of Silesia, 75 Pulku Piechoty 1A, 41-500 Chorzow, Poland
5Department of Chemistry, Laboratory of Inorganic Chemistry, University of Helsinki, P.O. Box 55, 00014 Helsinki, Finland

Correspondence should be addressed to Roman Nowak; nowak.roman5@gmail.com

Received 17 February 2016; Accepted 5 April 2016

Academic Editor: Jeffrey Elam

Copyright © 2016 Anna Majtyka et al. This is an open access article distributed under the Creative Commons Attribution License, which permits unrestricted use, distribution, and reproduction in any medium, provided the original work is properly cited.

The present paper pertains to mechanical properties and structure of nanocrystalline multiferroic BeFeO₃ (BFO) thin films, grown by atomic layer deposition (ALD) on the Si/SiO₂/Pt substrate. The usage of sharp-tip-nanoindentation and multiple techniques of structure examination, namely, grazing incidence X-ray diffraction, X-ray photoelectron spectroscopy, scanning electron microscopy, and energy dispersive X-ray spectrometry, enabled us to detect changes in elastic properties (95 GPa ≤ E ≤ 118 GPa) and hardness (4.50 GPa ≤ H ≤ 7.96 GPa) of BFO after stages of annealing and observe their relation to the material’s structural evolution. Our experiments point towards an increase in structural homogeneity of the samples annealed for a longer time. To our best knowledge, the present report constitutes the first disclosure of nanoindentation mechanical characteristics of ALD-fabricated BeFeO₃, providing a new insight into the phenomena that accompany structure formation and development of nanocrystalline multiferroics. We believe that our systematic characterization of the BFO layers carried out at consecutive stages of their deposition provides pertinent information which is needed to control and optimize its ALD fabrication.

1. Introduction

The BiFeO₃ compounds attract currently a significant interest due to their prominent multiferroicity that concerns their superior ferroelectric and (anti-)ferromagnetic properties. These fascinating materials give us a possibility to control ferroelectricity and ferromagnetism by means of a magnetic or electric field [1, 2]. Their magnetoelectric coupling and strong electric polarization raises the prospect of using these for data storage, magnetic detectors, and tunnel-junction devices or as essential spintronics materials [2–4].

There are numerous methods for production of BFO thin films, such as pulsed laser deposition (PLD) [5], metal-organic chemical vapor deposition (MOCVD) [6], radio frequency magnetron sputtering [7], or sol-gel solution deposition [8], to name merely a few. As is well known, the synthesis procedure has a pronounced effect on physical properties of different materials [9]; therefore establishing of a manufacturing process is very important. The present paper pertains to BFO thin films obtained via the atomic layer deposition (ALD) technique being nowadays widely appreciated due to, for instance, its capability to deposit various geometries with thickness control [10] or produce multiferroic materials with satisfying dielectric properties [11]. Thus, we employed the ALD procedure to obtain nanocrystalline BFO thin films which underwent nanomechanical probing, allowing us to investigate the mechanical properties and characterize the structure of our material, which is essential for technological applications of BFO [12, 13].

Although the electric and magnetic properties of BiFeO₃ compound are already well recognized [11], there is an increasing interest in mechanical properties of multiferroic
materials of industrial importance, especially in these produced in a nanostructured form [14]. Since the nanoindentation testing already proved to be a powerful tool to investigate this kind of materials [7, 8], we employed the surface-deformation measurements to reveal the relationship between mechanical behavior of BFO and its structure. Such an approach enabled one to conclude on elastic and plastic responses, stress-induced phase-transitions [15, 16], and dislocation-based mechanisms of nanodeformation in semiconductors and metals [15, 17], while the present paper demonstrates mechanical and structural changes in BFO produced via ALD, when various annealing times are used. Young modulus, hardness, and grain size of the material in question are determined. To our best knowledge, this study for the first time deals with the evaluation of multiferroic material properties during consecutive stages of its annealing process, until the crystalline BFO material is received.

2. Experimental

2.1. Material Synthesis and Preparation of the Samples. BiFeO$_3$ thin films were prepared by the ALD method using a process composed of two deposition stages. Firstly, deposition of initial Bi-O and Fe-O layers on an Si/SiO$_2$/Pt substrate was carried out at 413 K, using bismuth(III) 2,3-dimethyl-2-butoxide and iron(III) tert-butoxide as metal precursors. We applied an exact number of growth-cycles (200 cycles of iron oxide and 180 of bismuth oxide) followed by exposure of the material to water vapor in order to oxidize the deposited layers. This operation was repeated 15 times to achieve a satisfactory layered structure of Bi-O/Fe-O oxides. Secondly, the fabricated laminar “semiproducts” underwent annealing in nitrogen atmosphere at 823 K. The nonannealed samples were also secured for a further examination, for the sake of comparison. The duration of the applied thermal treatment varied for different sets of specimens denoted finally as S-5, S-30, and S-60 for the films annealed for 5, 30, and 60 minutes, respectively. Our multilayers were 500 nm thick, similar to those produced by Jalkanen et al., who considered only the S-60 material as the one with a well-developed BiFeO$_3$ crystalline structure (details in [11]).

2.2. Structural Analysis and Mechanical Testing. The crystalline structure of the ALD-prepared BFO material was determined by means of X-ray diffraction (PANalytical X’pert Pro diffractometer with CuK$_\alpha$ X-ray source, $\lambda = 1.5405$ Å) that enabled us to conclude on the grain size of the formed structure. The complementary evaluation of the obtained microstructure and the relative content of different elements were carried out using a Scanning Electron Microscope (SEM) equipped with an Energy Dispersive X-ray Spectrometer (EDS) within a Hitachi S-4800 (Oxford INCA 350 spectrometer) system. The quantitative analysis of composition of the obtained materials was made by means of X-ray Photoelectrons Spectroscopy (XPS) with monochromatized Al K$_\alpha$ radiation. In order to reveal the depth-distribution of investigated elements, Elastic Recoil Detection Analysis (ERDA) was employed to finally determine the structure of the ALD-produced BFO.

As far as the mechanical properties are concerned, we examined the prepared BFO materials using well-established nanoindentation experiments carried out with Hysitron Triboindenter TI 950 armed with a sharp diamond tip (Berkovich-type, radius of $R = 100$ nm) and alternatively a spherical one (radius of $R = 2 \mu$m). We intended to reveal changes in the mechanical response of the BFO multiferroic prior to and after the annealing process, in order to obtain a pertinent characteristic for the deposited material. Moreover, the nanoindentation results constitute a convenient supportive feedback for the control of the applied ALD fabrication process. We determined the essential mechanical parameters, namely, the elastic modulus $E$ and hardness $H$ of our films, according to the Oliver and Pharr method [20] with the central relationships that reads

$$H = \frac{P}{A},$$

$$\frac{1 - \nu^2}{E} = \frac{2\beta}{S\sqrt{\pi}} - \frac{1 - \nu^2}{E_i},$$

where $P$ is the indentation load, $A$ is projected contact area, $\beta$ is constant dependent on the tip geometry, $S$ is unloading stiffness, $\nu$ is film’s Poisson’s ratio, $\nu_i$ is Poisson’s ratio of a diamond, and $E_i$ is tip (diamond) elastic modulus, respectively.

Our nanoindentation experiments were carried out with a maximum load $P_{\text{max}}$ ranging from 200 to 1000\,$\mu$N in order to satisfy the commonly accepted practice that recommends refraining from exceeding the maximum indentation depth more than 10% of the investigated film thickness [21]. The selection of a smooth surface area, free of defects, and therefore suitable for nanoindentation measurements, was accomplished using Scanning Probe Microscopy (SPM) based on surface profiling by the tip being in contact with a film, which is available in our TI 950 instrument.

3. Results and Discussion

The structure of our ALD-grown materials was determined by grazing incidence X-ray diffraction. The examinations revealed a predominantly amorphous structure in the specimens that did not undergo the annealing process, while the others (namely, those heated for 5 min and longer) crystallized as a stable BiFeO$_3$-phase (Figure 1). A hexagonal $R3c$ (161) BFO structure with lattice constants of $a = b = 5.5876(3)$ Å and $c = 13.867(1)$ Å was detected. The two highest diffraction peaks recorded for the sample annealed for 5 minutes are broader and lower (Figure 1) than those observed for the film annealed for 60 minutes, which confirms a typical behavior of annealed polycrystals. The higher intensity suggests a higher content of the component generating the peak, in the present case, the increased amount of the BFO phase. The diffraction peaks at Bragg angle $\Theta = 39.9^\circ$ and $\Theta = 46.5^\circ$ correspond to Pt (III) and Pt (200) plane since our BFO samples were heterogeneously ALD-grown on a Si/SiO$_2$/Pt substrate. Interestingly, the spectrum recorded for S-60 reveals a smaller contribution of the Pt phase into the deposited BiFeO$_3$ film.
Moreover, the grain size of the crystallite was determined using Scherrer’s equation [22]:

\[ D = \frac{k\lambda}{\beta_w \cos \theta} \]  

where \( D \) is the crystallite size, \( k \) is a dimensionless shape factor, \( \lambda \) is the X-ray wavelength, \( \beta_w \) is the line width at half maximum intensity of the peak, and \( \theta \) is Bragg angle. Thus, the estimated grain size equalled 5.58, 10.06, and 8.66 nm for the annealed S-5, S-30, and S-60 samples, respectively.

The morphology of the deposited material was carefully examined by means of SEM-technique coupled with EDS analysis. The obtained micrographs (Figure 2) proved that the surface of the obtained specimens is homogeneous and smooth (see Figure 2). They also revealed a commonly expected increase of the grain size that occurs during the annealing process [7]. Interestingly, beyond the annealing-time-threshold of 30 minutes, we did not observe further changes in the surface morphology (Figure 2), and the structure seemed already well stabilized. This conclusion is supported by the results of the EDS measurements which enabled us to estimate the Bi/Fe content ratio of the examined samples (refer to Table 1). Thus, the stoichiometry proper for BiFeO₃ was confirmed exclusively in the case of the S-60 material.

The results of the XPS examinations revealed a principal core level of Bi, Fe, and O ion content and confirmed the presence of C, F, and Si in the samples structure. The spectra were corrected for the background signal using the iterated Shirley algorithm, while the band levels were adjusted using Gaussian and Lorentzian lines. The presence of characteristic spectral lines for Fe2p core levels (Figure 3(a)) proved that FeO with binding energy of \( E_b = 709.9 \) eV and Fe₃O₄ (\( E_b = 710.8 \) eV) are included among the main components of our film. The same applies to the Bi4f (Figure 3(b)) core level and consequently to the Bi₂O₃ phase (\( E_b = 158.95 \) eV). The satellite peak for Fe³⁺ (Figure 3(a)) located at 719 eV suggests a partial oxidation of our samples, which is in accordance with the observation by Li et al. [23]. Despite considerable difficulties in detection of the contribution from the Fe and Bi oxide from the OIs core level (Figure 3(c)), we successfully determined the binding energy of 529.85 eV for both Bi and Fe oxides using the NIST database. Furthermore, the SiO₂ signal from the substrate that we used for BFO deposition was also registered. Thus, the investigation of chemical state of our material confirmed the presence of pure BFO phase.

For the sake of clarity of our paper, we carried out the indentation examination for the nonannealed (S-0) and long-annealed (S-60) BFO thin films only. Our SPM probing of the surface of the nonannealed (Figure 4(a)) and annealed (Figure 4(b)) specimens revealed a significant difference in the surface morphology. The nanoindentation measurements were carried out on a carefully selected area of the samples with a similar roughness. It was possible due to the nanometer-scale contact area induced by our indenter. Thus, our nanoindentation results can be considered as virtually unaffected by the displayed surface features (Figures 4(a)-4(b)).

The micrographs in Figures 4(a) and 4(b) disclose a difference in the surface roughness for the nonannealed and annealed specimens. However, the marked consistency and repeatability of the obtained results (refer to Figure 4(c)) convince us that the noted discrepancies do not affect the results of mechanical testing. Consequently, we reported a considerable change in mechanical properties of the BFO specimen when annealed for a longer time (compare black and red curves in Figure 4(c)). Despite the character of the \( P-h \) curves being of a similar kind, the material after

<table>
<thead>
<tr>
<th>Sample</th>
<th>Bi/Fe ratio</th>
</tr>
</thead>
<tbody>
<tr>
<td>Nonannealed</td>
<td>1.07 ± 0.02</td>
</tr>
<tr>
<td>5 min</td>
<td>1.03 ± 0.02</td>
</tr>
<tr>
<td>30 min</td>
<td>1.04 ± 0.02</td>
</tr>
<tr>
<td>60 min</td>
<td>0.97 ± 0.02</td>
</tr>
</tbody>
</table>

**Table 1**: The Bi/Fe ratio concluded from EDS measurements carried out for BiFeO₃ thin films.
the thermal treatment (S-60) becomes markedly harder (a significantly lower indentation depth $h$) than the ALD-grown one (S-0), which runs contrary to common expectation (Figure 4(c)). Indeed, polycrystalline materials (especially metals) usually turn softer after annealing [7], which contrasts with the discovered BFO behavior. All of these bring us to suspect that the observed hardening is due to considerable structural changes which occur during annealing.

The deformation of the amorphous material (S-0, black curve) and the one crystallized during annealing (see Figure 4) of the BFO films (S-60, red curves) performed within a load range from $P_{\text{max}} = 200 \mu \text{N}$ to $1000 \mu \text{N}$ does not resemble either the results obtained for GaN [15] and GaAs [16] crystals, in which nanodeformation depends on the transition between crystalline structures, accompanied by a dislocation activity.

Our analysis of the nanoindentation $P-h$ data is supported by classical hardness and elastic modulus measurements that confirm that the heat treatment resulted in increase of these two. Furthermore, the results of our nanomechanical testing were compared with those obtained by other authors for different deposition methods and various kinds of measurements, or they were predicted theoretically (Table 2). Thus, we contend that the nanoindentation probing and the recorded mechanical characteristics serve to be a convenient indicator of the process that undergoes between Bi-O and Fe-O layers with increasing time of heat treatment.

Our results reveal a decrease in hardness and elastic moduli with an increasing load, which reflects the well-known “size effect” [24]. The corresponding Young modulus values (hardness) for BFO material are $118.31 \text{ GPa (7.96 GPa)}$, $114.43 \text{ GPa (7.80 GPa)}$, and $111.11 \text{ GPa (7.50 GPa)}$ for loads

---

**Table 2: Elastic modulus and hardness of S-0 and S-60 BFO thin films obtained from different deposition methods.**

<table>
<thead>
<tr>
<th>Method</th>
<th>$E$ (GPa)</th>
<th>$H$ (GPa)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Atomic layer deposition (ALD)</td>
<td>111.11–118.31</td>
<td>7.50–7.96</td>
</tr>
<tr>
<td>Radio frequency magnetron sputtering [7]</td>
<td>131.4–170.8</td>
<td>6.8–10.6</td>
</tr>
<tr>
<td>Sol-gel [8]</td>
<td>26–51</td>
<td>2.8–3.8</td>
</tr>
<tr>
<td>Pulsed laser deposition [18]</td>
<td>100</td>
<td>—</td>
</tr>
<tr>
<td></td>
<td>C-AFM - 144.87</td>
<td>—</td>
</tr>
</tbody>
</table>

---

Figure 2: SEM micrographs of BFO films after annealing at $T = 300 \text{ K}$ for 0, 5, 30, and 60 min (the samples denoted as S-0, S-5, S-30, and S-60). The insets (c and d) reveal structural aspects in a greater detail, which disclose a difference between the S-60 sample (d) which contains BiFeO$_3$ structure (refer to Figure 1) and the other materials (a, b, c).
Figure 3: XPS spectra obtained for a 500 nm BiFeO$_3$ film (S-60) grown by the ALD technique. One can readily recognize the spectral components for Fe2p (a), Bi4f (b), and also O1s lines (c).

(depths) of 200 $\mu$N (25 nm), 600 $\mu$N (52 nm), and 1000 $\mu$N (76 nm), respectively.

One should note that hardness of the nonannealed sample ($H = 4.5$ GPa) is almost two times lower than that of the one which underwent the annealing procedure, and its elastic modulus is also lower (95 GPa).

4. Conclusions

The present work focused on the relationship between mechanical characteristics and structure of industrially important multiferroic BiFeO$_3$ films ALD grown on an Si/SiO$_2$/Pt substrate and subsequently variously annealed. This way, we revealed a dependence of the common mechanical parameters on the stage of crystallization of BFO films and finally formation of the BiFeO$_3$ structure. Thus, we contend that nanoindentation constitutes a simple and very convenient method of testing multiferroic films with respect to formation of a properly developed structure of the material.

In a greater detail, a number of measurements were carried out to determine both structure and mechanical properties of the BFO thin film that underwent a post-ALD thermal treatment (annealing) at 823 K which lasted for 5, 30, and 60 minutes. The as-deposited samples (S-0) were also examined as a reference material. Thus, the structures of the samples labelled as S-0, S-5, S-30, and S-60 were extensively investigated by means of XRD, XPS, SEM, and EDS techniques.

Since we found that our ALD-grown BFO layers require at least 60 minutes of treatment to crystallize in the intact
BiFeO$_3$ structure, the mechanical testing was limited to as-deposited (S-0) and final (S-60) state proving that the nanoindentation testing is a perfect experimental method to provide us the information about the stage of formation of a multiferroic material.

Furthermore, our research provides (to the best of our knowledge for the first time) nanoindentation mechanical characteristics of BFO multiferroics grown by means of the ALD process. Hardness obtained under nominal loads of 200, 600, and 1000 $\mu$N was equal to 7.96, 7.80, and 7.50 GPa, respectively (please note that hardness is a load-dependent material property that reflects plastic properties of the material) [25]. In contrast hardness of the as-deposited film amounted to 4.5 GPa. As for elastic characteristics, the level elastic moduli of a properly crystallized BiFeO$_3$ equalled 118.31, 114.43, and 111.11 GPa under various loads, while that of the as-grown material (S-0) approached ~95 GPa. The almost negligible load/depth-dependence of $E_r$ - and $H$ -parameter of our sample proved a homogeneity of the material and correctness of our measurements.

**Competing Interests**

The authors declare that they have no competing interests.

**Acknowledgments**

The authors thank the Academy of Finland for the support through the Research Consortium PROPER within the Finnish Research Program for PROGRAMABLE MATERIALS (OMA) and the Finnish Centre of Excellence in Atomic Layer Deposition. Dariusz Chrobak acknowledges support...
from the National Science Center of Poland under Grant number DEC-2012/05/B/ST-8/02945.

References


